

From last time

$$c(x) \rho(x) \frac{\partial u(x,t)}{\partial t} = \frac{\partial}{\partial x} \left( k_0(x) \frac{\partial u}{\partial x} \right) + Q(x,t)$$

Heat equation that we study:

\* General heat equation for a 1-D conducting rod.

$$c(x) \rho(x) \frac{\partial u(x,t)}{\partial t} = k_0 \frac{\partial^2 u(x,t)}{\partial x^2}$$

Even simpler assume  $c=c(x)$  and  $\rho=\rho(x)$  are also const.

$$c \rho \frac{\partial u(x,t)}{\partial t} = k_0 \frac{\partial^2 u(x,t)}{\partial x^2}$$

Thus

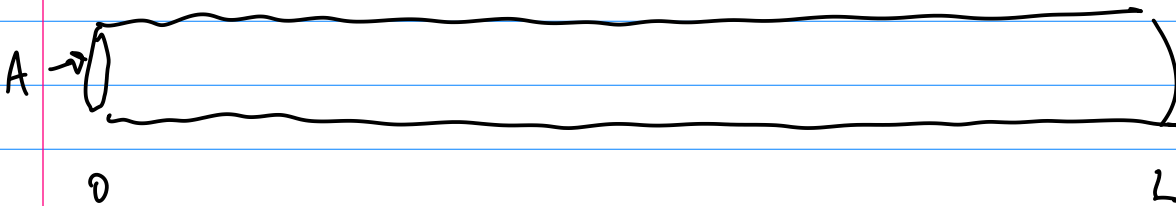
$$\frac{\partial u}{\partial t} = \kappa \frac{\partial^2 u}{\partial x^2}$$

$$\text{where } \kappa = \frac{k_0}{c \rho}.$$

simplest heat equation.

diffusivity  
rate of diffusion of the heat.

Conducting rod



- physically need to know what happens at the ends of the domain,  $x=0$  and  $x=L$
- what was the initial temperature distribution in the rod,

Physical units in this problem

$$\frac{\partial u}{\partial t} = k \frac{\partial^2 u}{\partial x^2}$$

$$\frac{\partial u}{\partial t} \sim \frac{[u]}{[T]}$$

$$\frac{\partial^2 u}{\partial x^2} \sim \frac{[u]}{[L]^2}$$

$$k \sim \frac{[u]}{[T]} / \frac{[u]}{[L]^2} = \frac{[L]^2}{[T]}$$

diffusivity  
rate of diffusion of the heat

$$k = \frac{k_0}{c \rho} = \frac{\frac{[E]}{[M][L][u]}}{\frac{[E]}{[M][u]} \frac{[M]}{[L]^3}} = \frac{[L]^2}{[T]}$$

dimensional consistency  
as these are the same...

What are the dimensions of  $k_0$ ?

$$q(x, t) \sim -k_0(x) \frac{\partial u}{\partial x}$$

$$q \sim \frac{[E]}{[T][L]^2}$$

$$\frac{[E]}{[T][L]^2} = [k_0] \frac{[u]}{[L]}$$

$$k_0 \sim \frac{[E]}{[T][L]^2} / \frac{[u]}{[L]} = \frac{[E]}{[M][L][u]}$$

• The PDE  $\frac{\partial u}{\partial t} = k \frac{\partial^2 u}{\partial x^2}$

• The initial conditions.

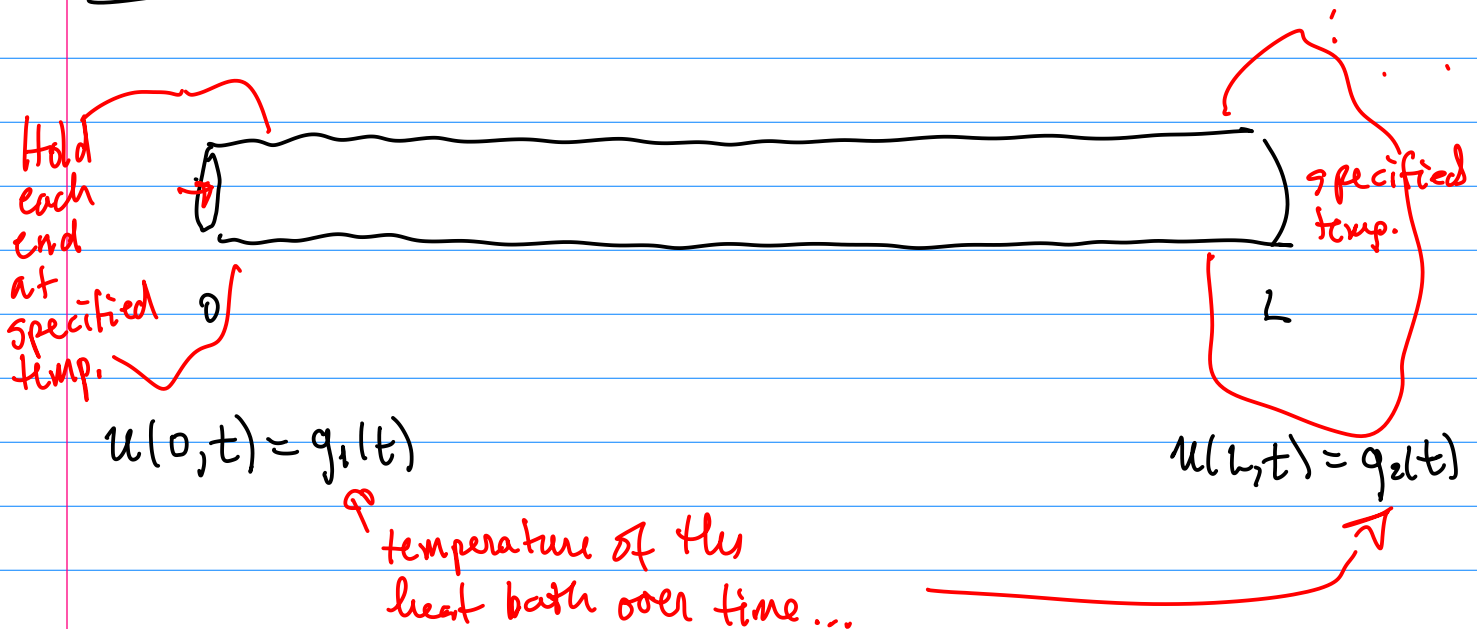
• The boundary condition

Initial conditions: specify the distribution of heat

for example,  $u(x, 0) = f(x)$  for  $x \in [0, L]$   
*initial distribution of heat*

Boundary Condition:

Heat Bath:



Insulated boundary condition . No flux at the boundary

$$q(0, t) = 0$$

and

$$q(L, t) = 0$$



No flux of heat energy through the boundary.

Since

$$q(x, t) = -k_0(x) \frac{\partial u}{\partial x}$$

$$0 = q(0, t) = -k_0(0) \frac{\partial u}{\partial x} \Big|_{x=0} = 0$$

$x=0$

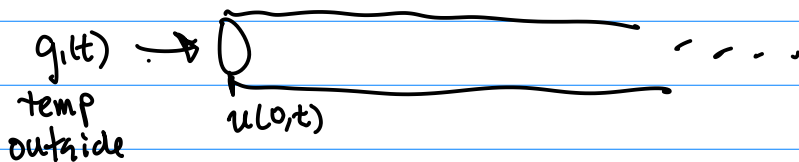
$$\text{thus } \frac{\partial u}{\partial x} \Big|_{x=0} = 0$$

In terms of temperature insulated boundary conditions.

$$\frac{\partial u}{\partial x} \Big|_{x=0} = 0 \quad , \quad \frac{\partial u}{\partial x} \Big|_{x=L} = 0$$

## Newton's Law of Cooling

and rod temperatures). Experiments show that, as a good approximation, the heat flow leaving the rod is proportional to the temperature difference between the bar and the prescribed external temperature. This boundary condition is called **Newton's law of cooling**. If it is valid at  $x=0$ , then



$$-k_0 \frac{\partial u}{\partial x} \Big|_{x=0} = q(0, t) = H_1 (q_1(t) - u(0, t))$$



$$-K_0 \left. \frac{\partial u}{\partial x} \right|_{x=L} = \phi(L,t) = H_2 (u(L,t) - q_2(t))$$

Goal: predict the future.

Simpler Goal: predict super far into the future as  $t \rightarrow \infty$ .

Idea: as  $t \rightarrow \infty$  the heat distribution enters into an equilibrium state provided none of the boundary terms have an explicit time dependence.

For example the heat bath...

$$\begin{array}{ccc}
 u(0,t) = q_1(t) & & u(L,t) = q_2(t) \\
 \uparrow & & \uparrow \\
 \text{temp at} & & \text{temp of} \\
 \text{left} & & \text{right bath} \\
 & \text{constant interface} & \\
 q_1(t) = q_1 & & q_2(t) = q_2 \\
 q_2(t) = q_2 & & \\
 u(0,t) = q_1 & & u(L,t) = q_2
 \end{array}$$

If in equilibrium then  $\frac{\partial u}{\partial t} = 0$  so the heat equation reduces to

Solve this next time:  $0 = k \frac{\partial^2 u}{\partial x^2}$